



Optimized common mode chokes for high current applications

SEKELS GmbH

Optimized common mode chokes for high current applications

- | basics and definitions
- | alloys
- | winding
- | contacting
- | mechanical aspects
- | behavior under nominal current

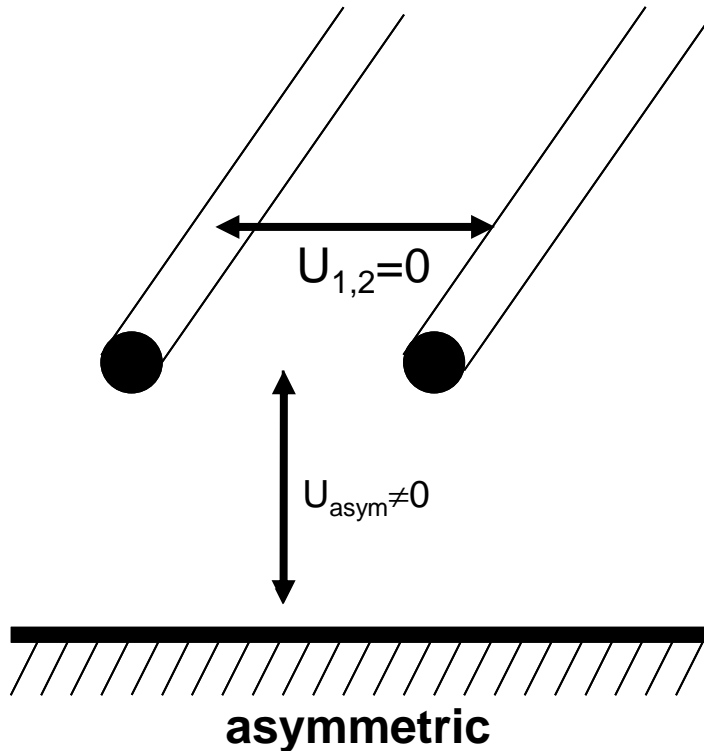


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Definition: Noise voltages

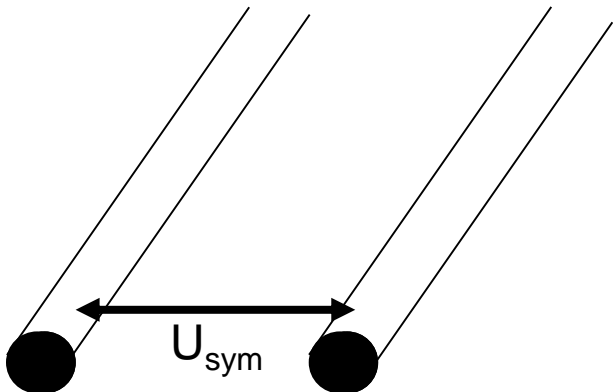
● Common mode (asymmetric noise voltage)



- no potential difference between the conductors.
- common potential difference between ground and conductors.
- occurs mostly at low frequencies.
- attenuation by nominal inductance of a common mode choke

Definition: Noise voltages

● Differential mode (symmetric noise voltage)

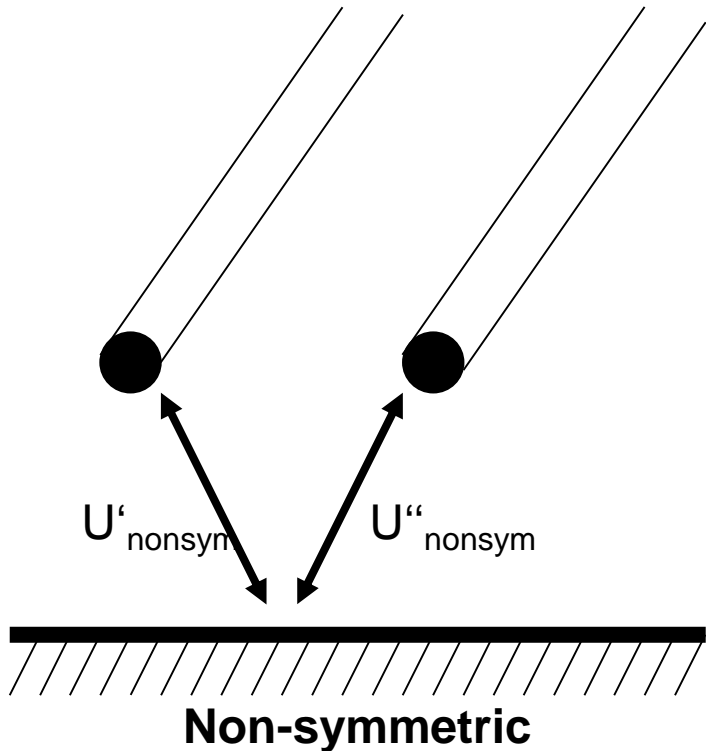


- potential difference between the conductors
- occurs mostly at high frequencies (>1 MHz).
- attenuation mainly by leakage inductance of common mode choke (if necessary with additional linear choke).



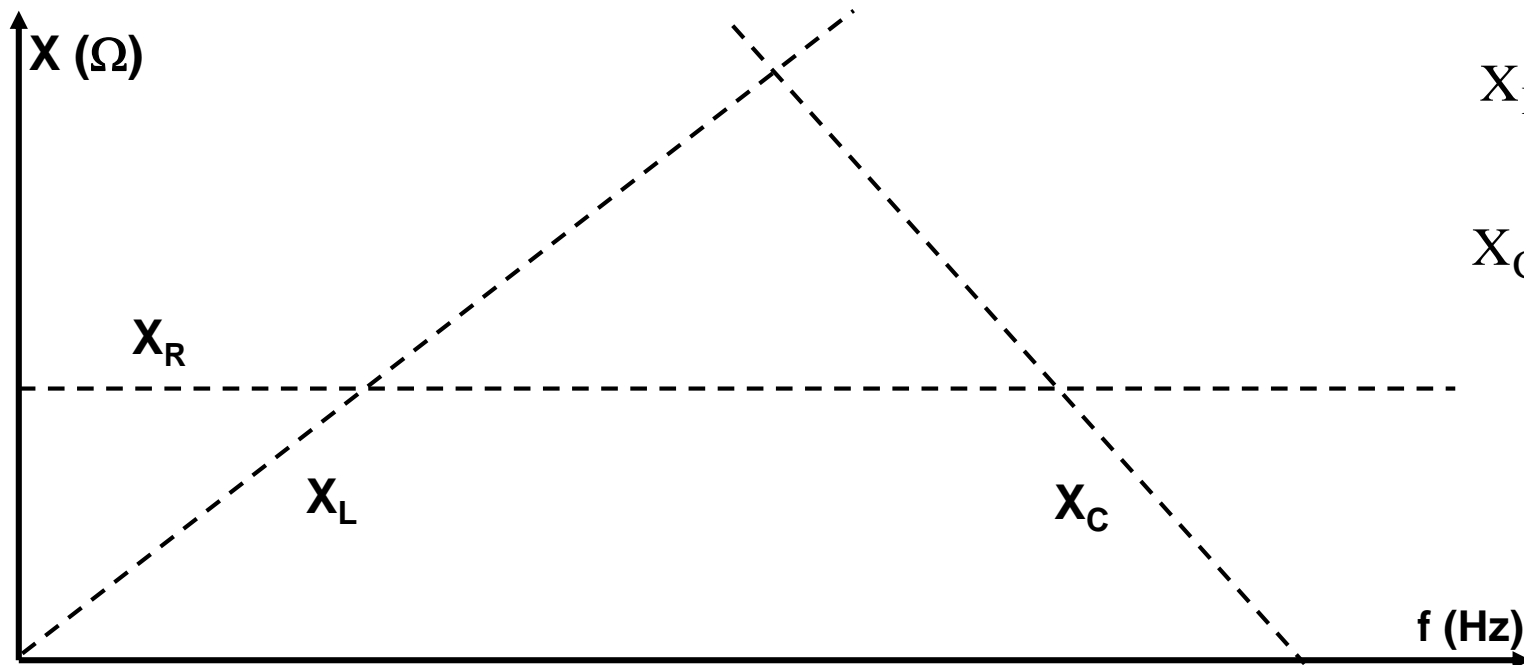
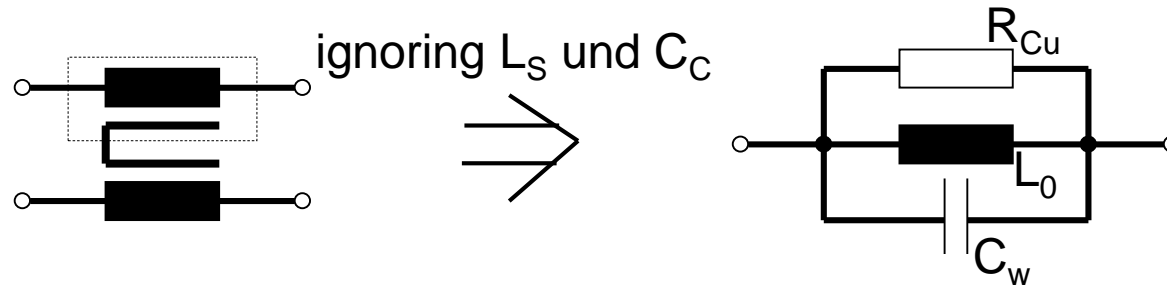
Definition: Noise voltages

● Common mode interference (non-symmetric noise voltage)



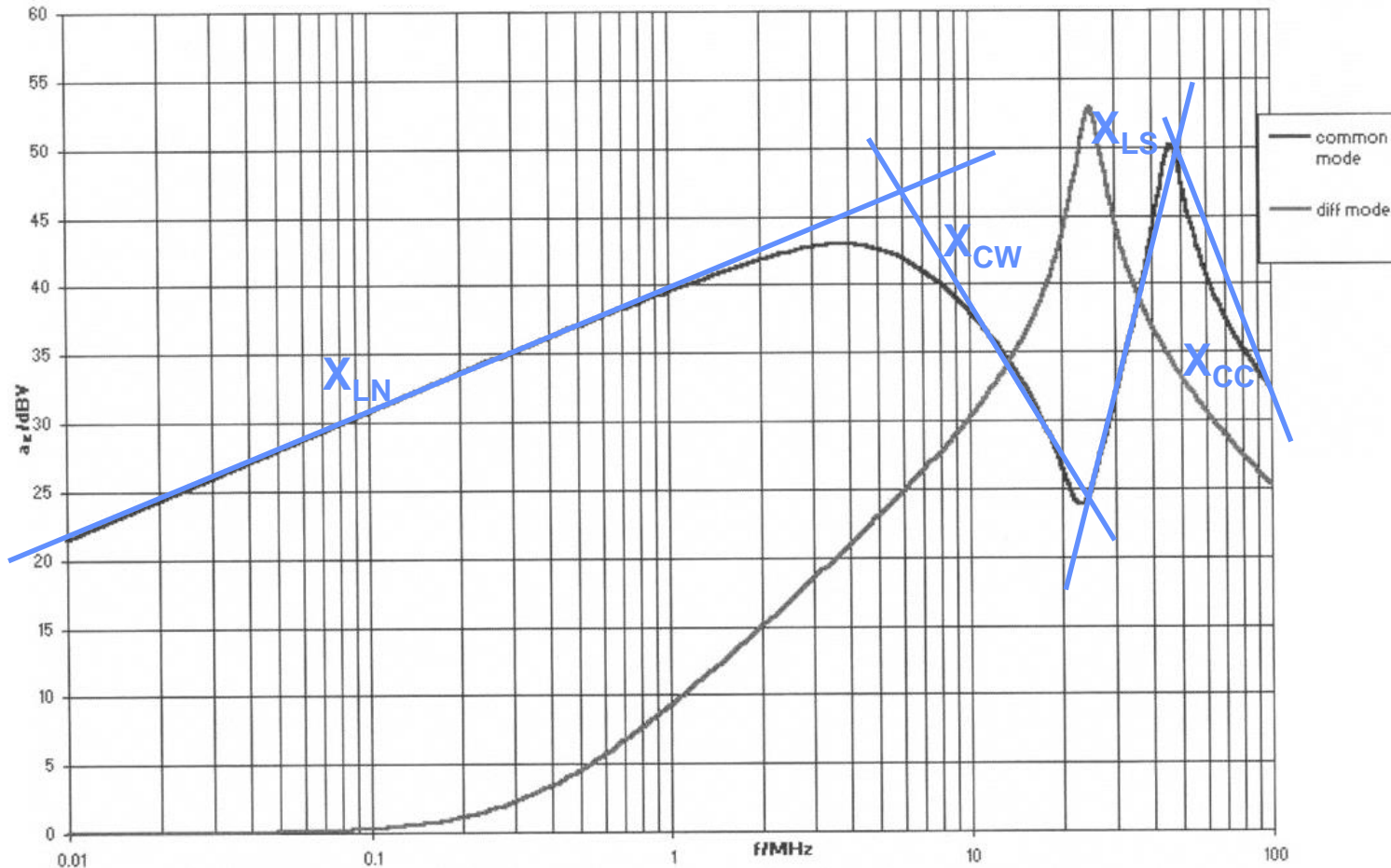
- noise voltage applies between conductors and ground.
- different potential differences for each conductor.
- attenuation by nominal inductance

Simplified equivalent circuit for common mode chokes



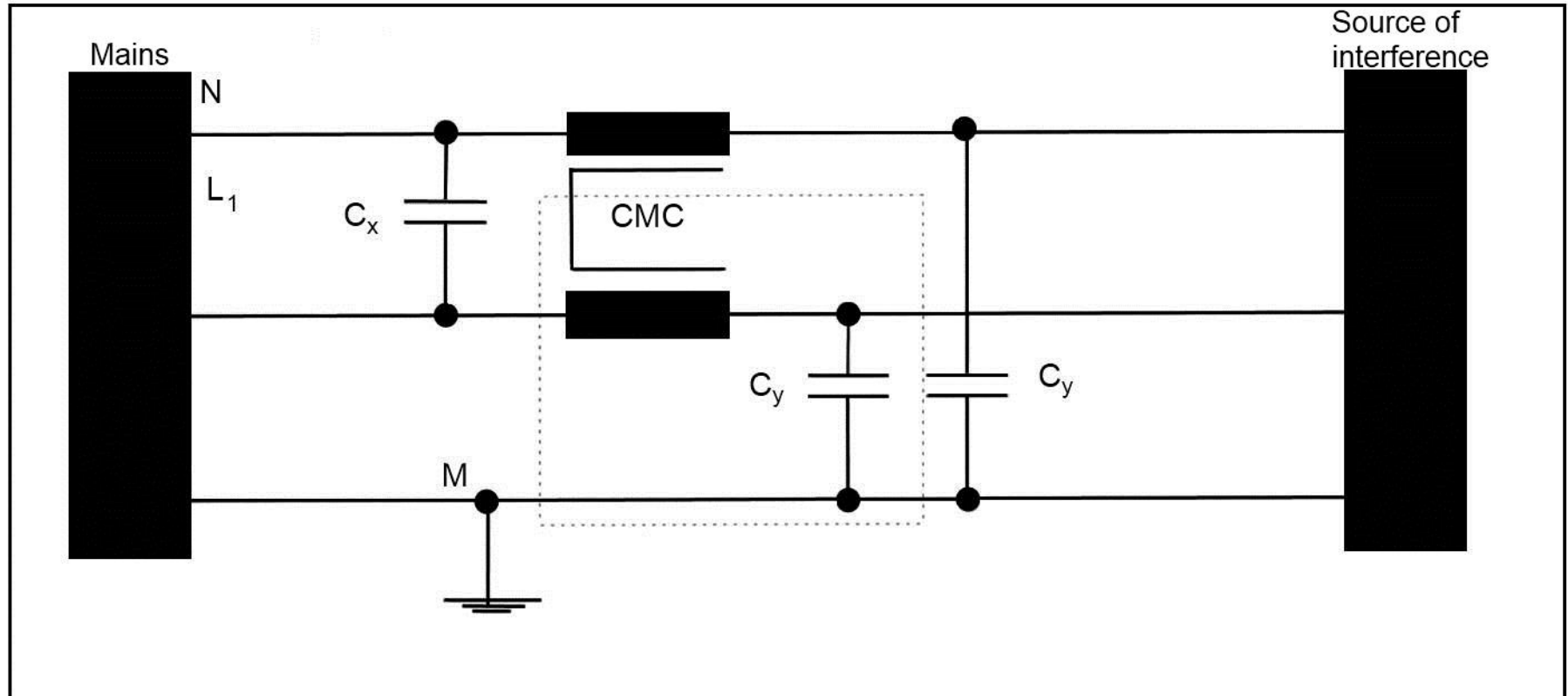
Damping behavior

Permeability ≥ 70.000 Core Dimensions 40x32x15 Windings: N=20



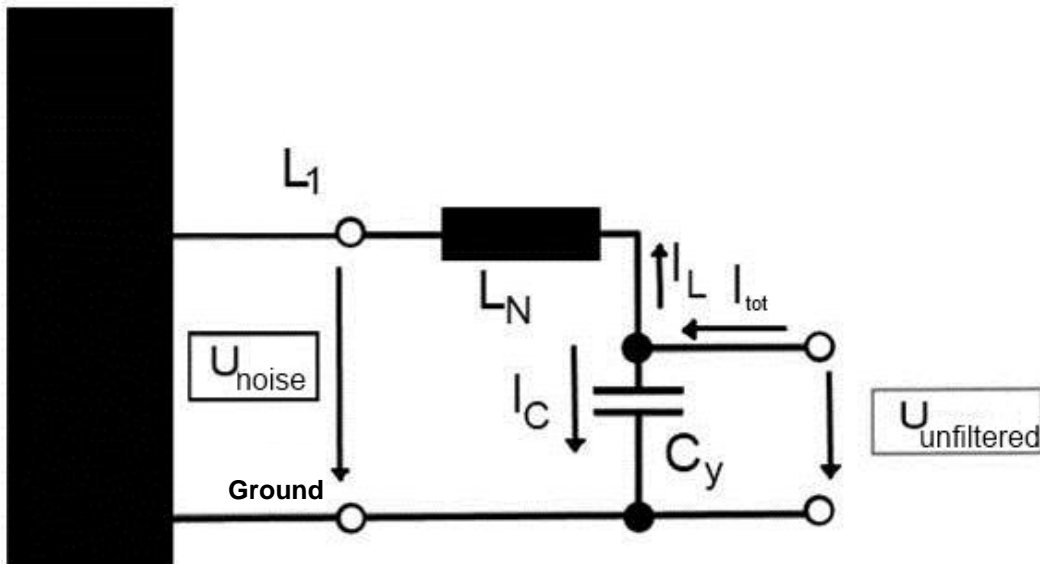
Basic circuit

Common mode choke in filter



Basic circuit

Common mode choke in filter



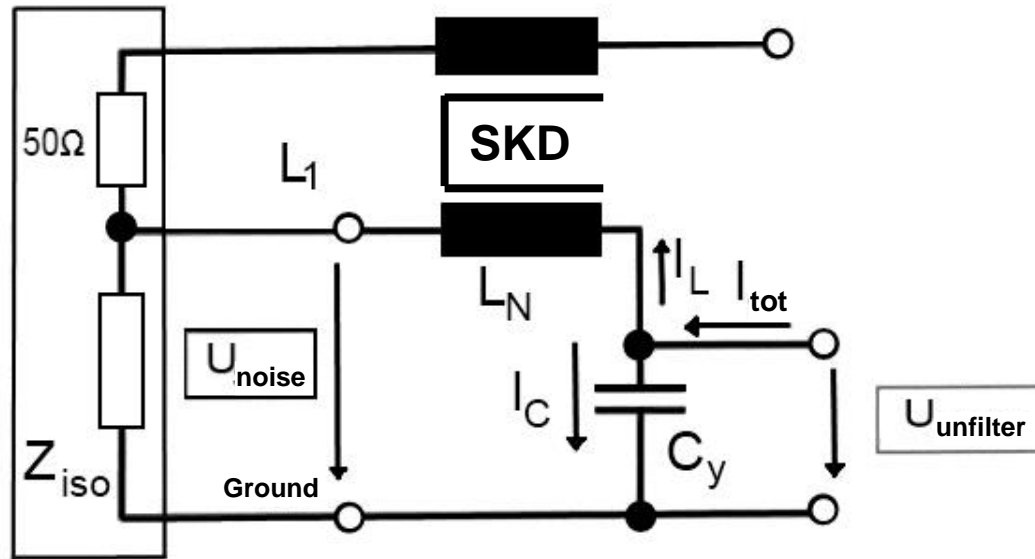
The unfiltered noise voltage is split according to the impedances $Z_{tot.} = Z_L + Z_C$.

If Z_C is small compared to Z_L the main part of the noise currents are directed to the ground via C_y . This results in a small U_{noise} .

C_y may not be chosen arbitrarily large, so a high choke impedance Z_L is desired.

Basic circuit

Common mode choke in filter

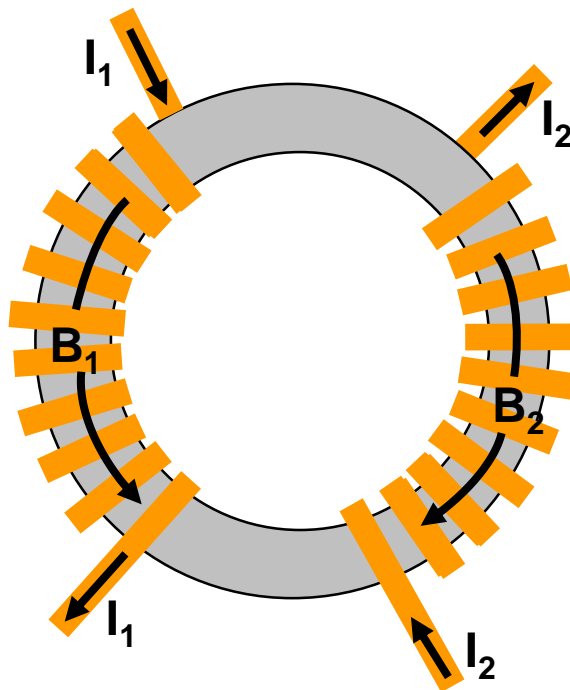


The symmetric part I_{sym} compensates itself, because it flows through both windings of the choke. The core is not saturated.

The asymmetric part I_{asym} is directed to the ground via Z_{iso} and Z_{Cy} . The voltage divider consisting of Z_L and Z_C limits the saturation current of the choke.

Structure and principle of a common mode choke

Basic structure:



Structure:

- Core (tape-wound-core, ferrite, powder-core etc.)
- Copper winding (litz, round massive wire, flat bar wire)

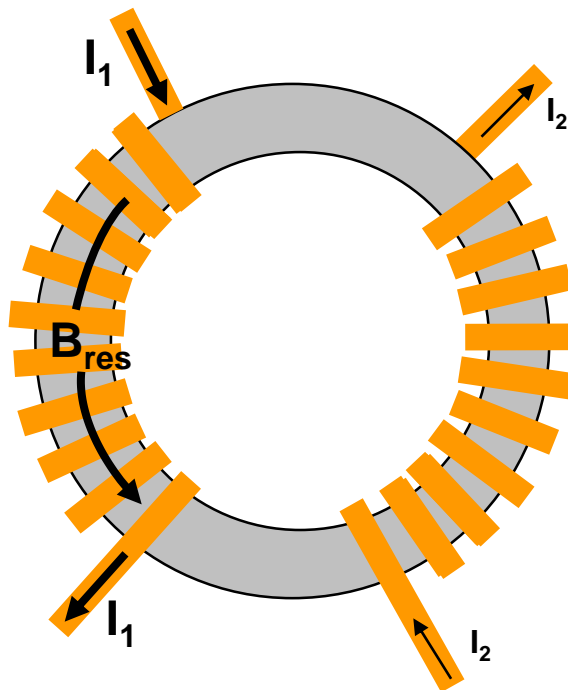
Principle (simplified):

Winding 1 and 2 are energized in opposite directions.

- CMC offers inductance.
- noise currents are directed to ground via y-capacitor.

Structure and principle of a common mode choke

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Principle (simplified):

Winding 1 and 2 are energized in opposite directions.

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Saturation of the choke:

- high non-symmetric currents lead to a resulting magnetization in the core => saturation
- efficiency of voltage divider (CMC and y-capacitor) reduced drastically.

What to do if the choke saturates?

- reduce N?

Magnetic induction $B = \mu_0 \cdot \mu_r \cdot H = \mu_0 \cdot \mu_r \cdot \frac{N \cdot I}{l_{Fe}}$ „Saturation“ $\sim N$

Inductance $L = N^2 \cdot A_L = N^2 \cdot \mu_0 \cdot \mu_r \cdot \frac{A_{Fe}}{l_{Fe}}$ Inductance $\sim N^2$

⇒ No improvement, even worse filtering properties! 😞

- reduce permeability?

Saturation $\sim \mu_r$

Inductance $\sim \mu_r$

⇒ Improvement possible, worth a try! 😊

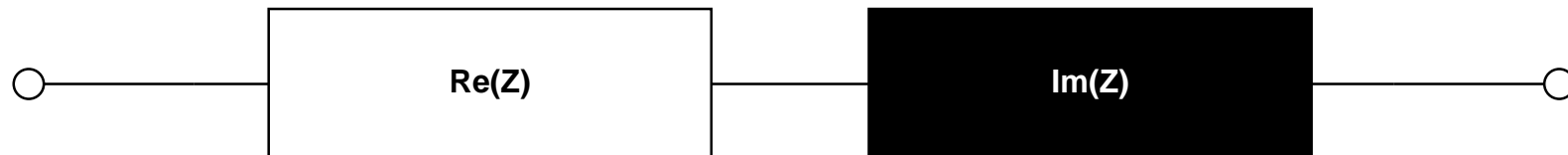
Equivalent circuit - μ' , μ''



Equivalent circuit - μ' , μ''

Insertion damping:

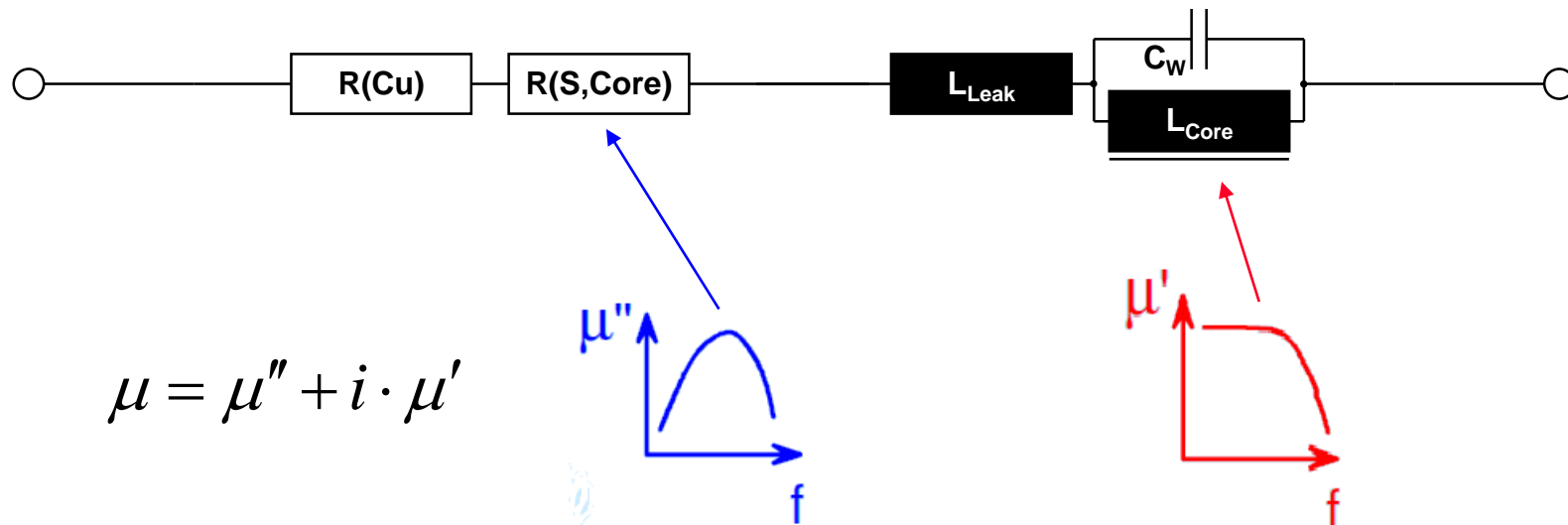
$$|Z| = \sqrt{(\operatorname{Re}(Z))^2 + (\operatorname{Im}(Z))^2} \approx \sqrt{R_{S,Core}^2 + (\omega \cdot L_{Core})^2}$$



Equivalent circuit - μ' , μ''

Insertion damping:

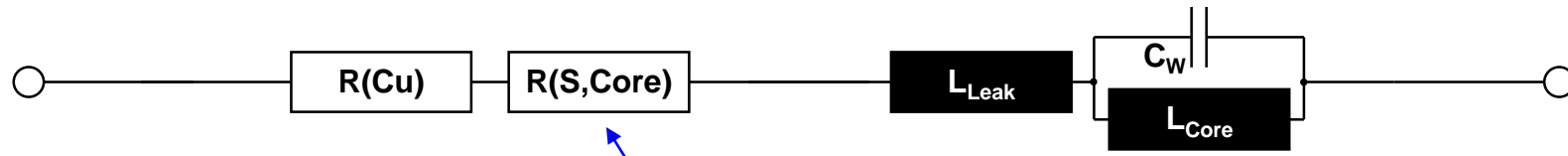
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Equivalent circuit - μ' , μ''

Insertion damping:

$$|Z| = \sqrt{(\operatorname{Re}(Z))^2 + (\operatorname{Im}(Z))^2} \approx \sqrt{R_{S,Core}^2 + (\omega \cdot L_{Core})^2}$$



$$L_{Core} = \mu_0 \cdot \mu'_S \cdot N^2 \cdot \frac{A_{Fe}}{l_{Fe}}$$

$$R_{S,Core} = \omega \cdot \mu_0 \cdot \mu''_S \cdot N^2 \cdot \frac{A_{Fe}}{l_{Fe}}$$



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Core alloy

**Amorphous &
nanocrystalline**



Iron powder



Silicon iron (3%, 6%)

Ferrite



Core alloy

Advantages and disadvantages of different alloys

Material	Good	Bad
Amorphous	Good saturation, good permeability, thin layers	Magnetostriction, (corrosion)
Nanocrystalline	Highest permeability, good saturation, hardly any magnetostriction, very low losses, different hysteresis loops possible	Not the cheapest
NiFe	High permeability	Low saturation, not the cheapest
Ferrite	Isotropic behavior, cheap	Low saturation, high temperature dependence
Fe- Powder	High saturation, Isotropic behavior	Magnetostriction, corrosion, low permeability
SiFe (laminated)	Highest saturation	Thickness, magnetostriction, corrosion, low permeability

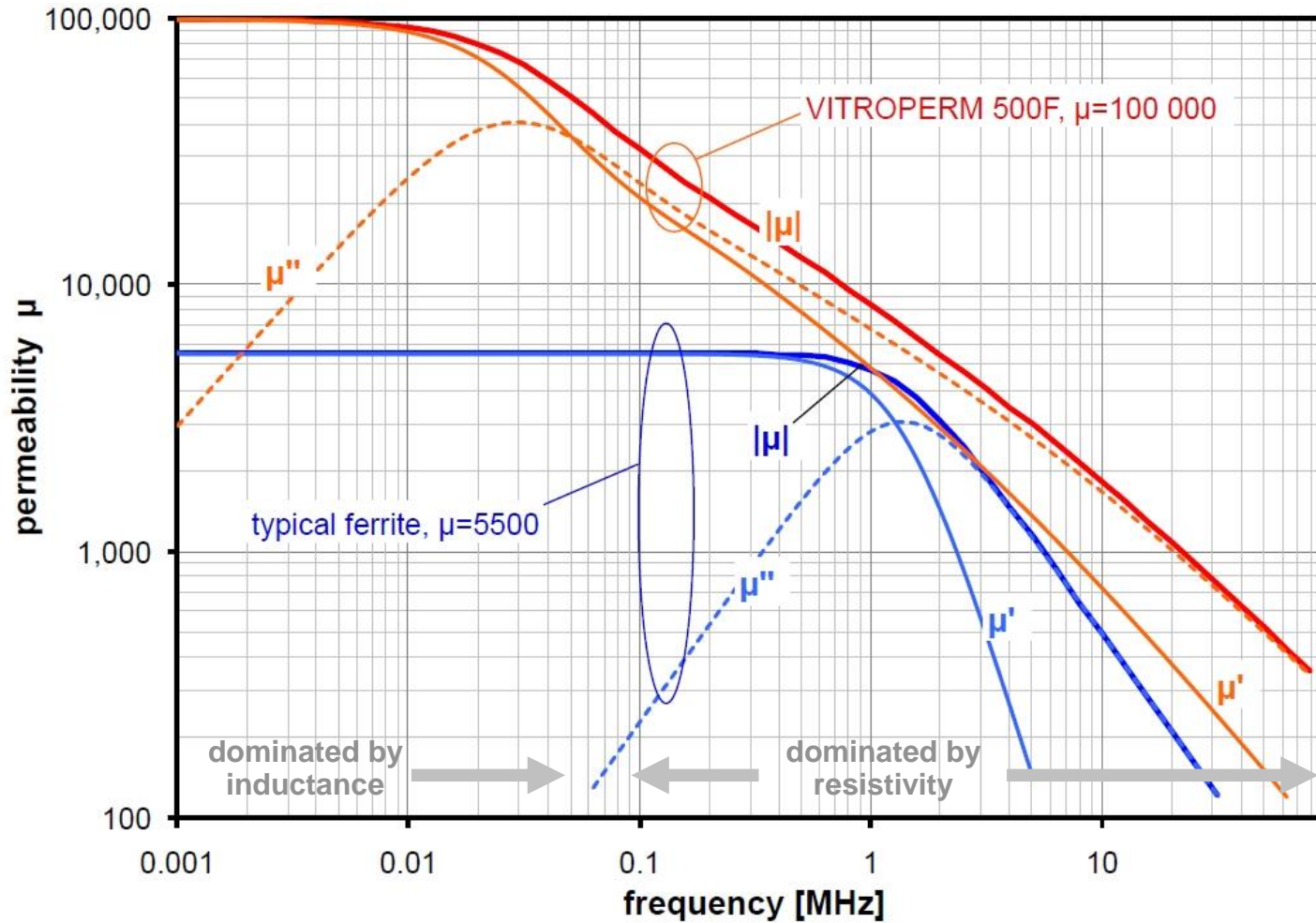
Core alloy

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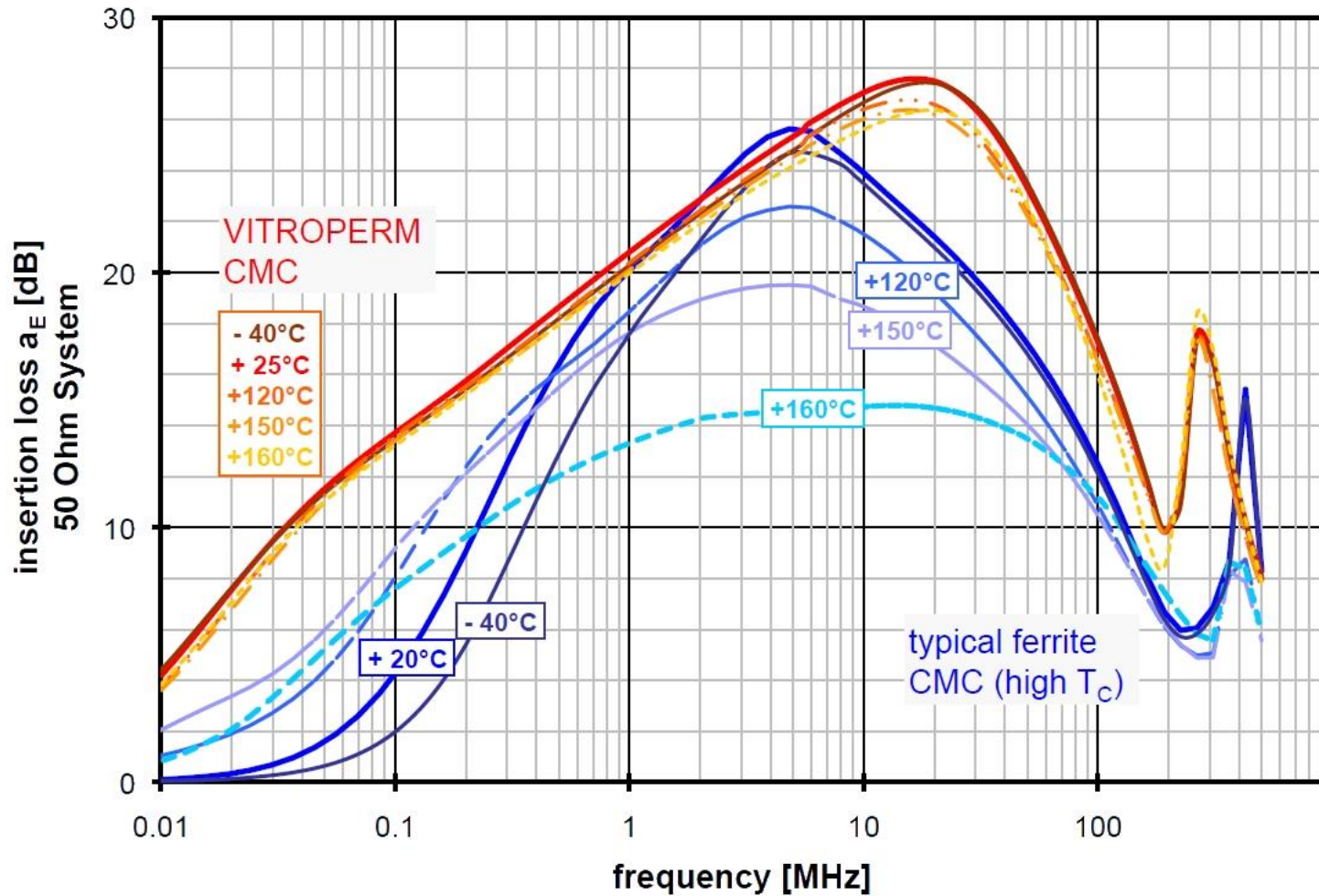
Core alloy

Frequency dependence of the permeability



Core alloy

Temperature dependence of the permeability



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Winding

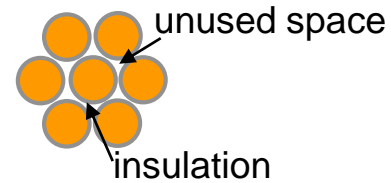
Advantages and disadvantages of several conductor types

Litz

+ easy to wind



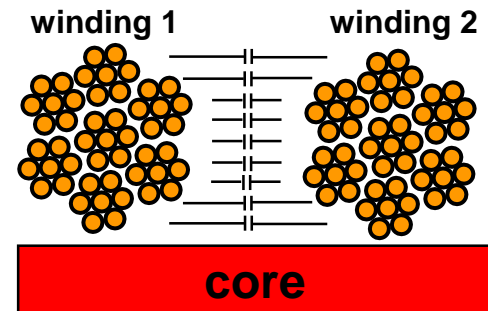
- bad fill factor



+ easy to contact



- bad hf properties (C_W)



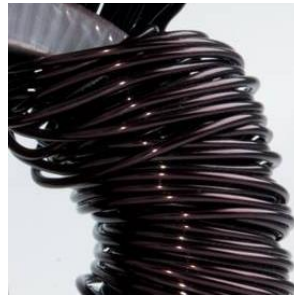
Winding

Advantages and disadvantages of several conductor types

● Massive round wire

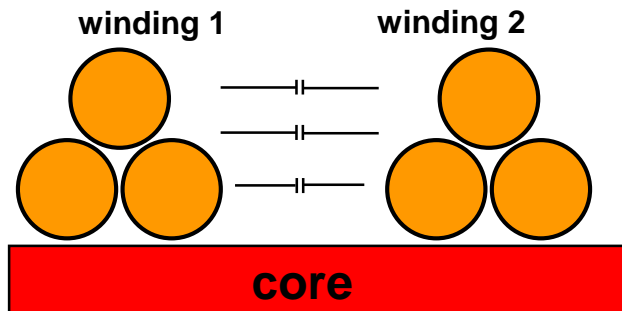
+ good fill factor

- difficult to wind



+ good hf behavior

- special contacting necessary



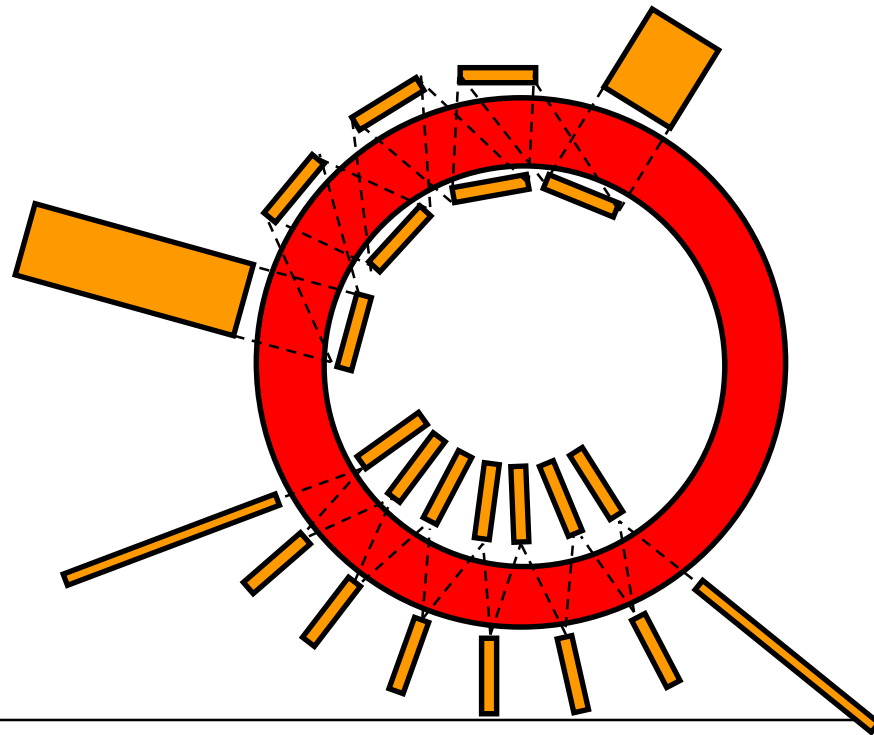
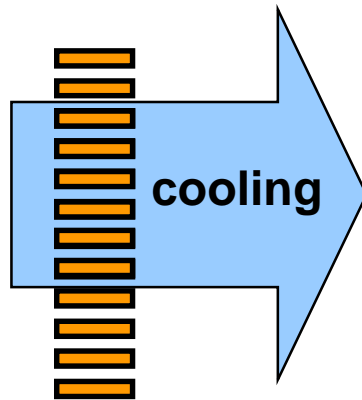
Winding

Advantages and disadvantages of several conductor types

● Flat bar wire

+ high current density

- bad fill factor (for round cores)
- special winding technique



Winding with litz wire

$I_N = 220 \text{ A}$; $L = 2 \times 290 \mu\text{H}$

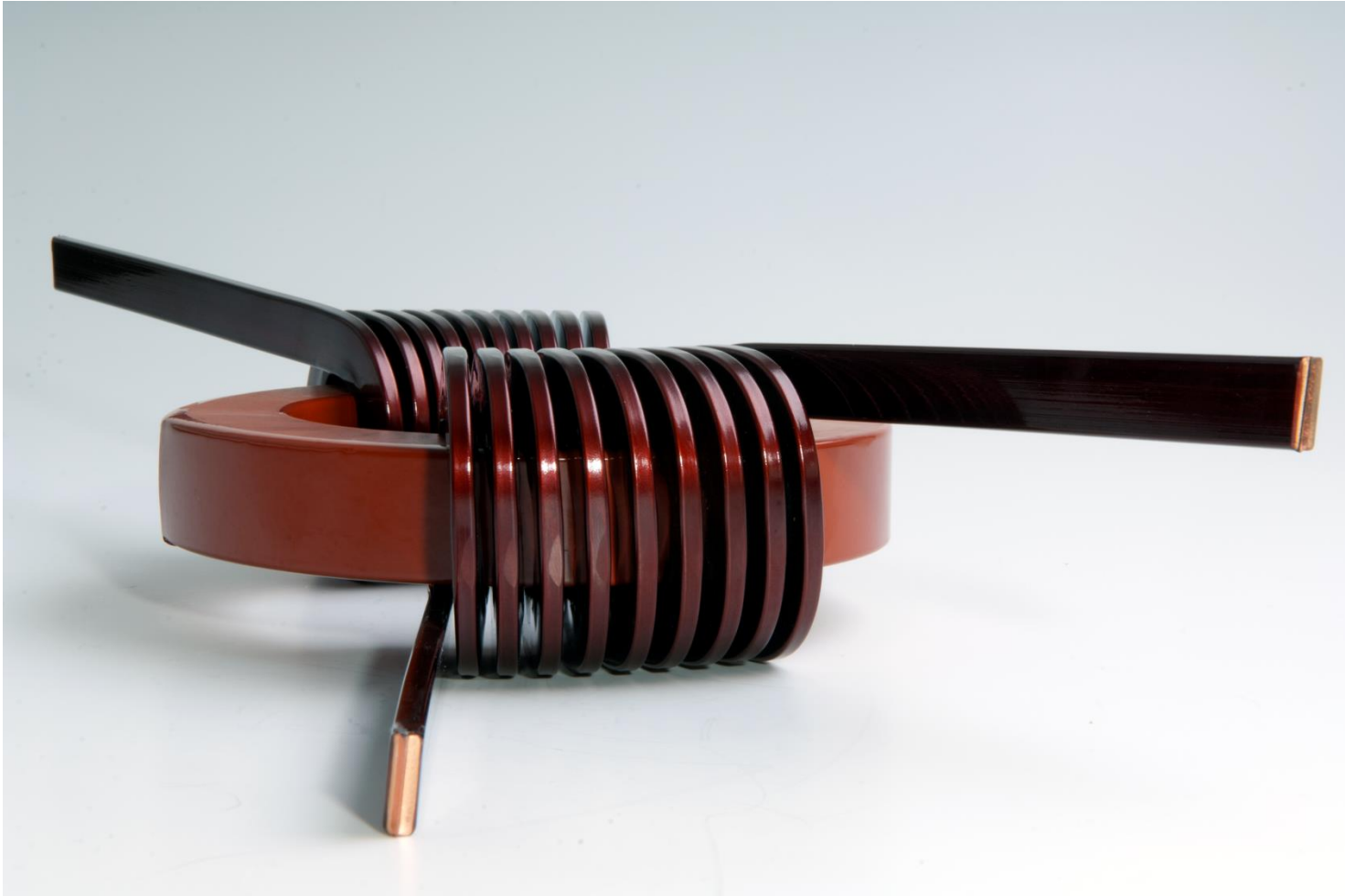


Winding with massive round wire

$I_N=500\text{ A}$; $L= 2 \times 1000\ \mu\text{H}$

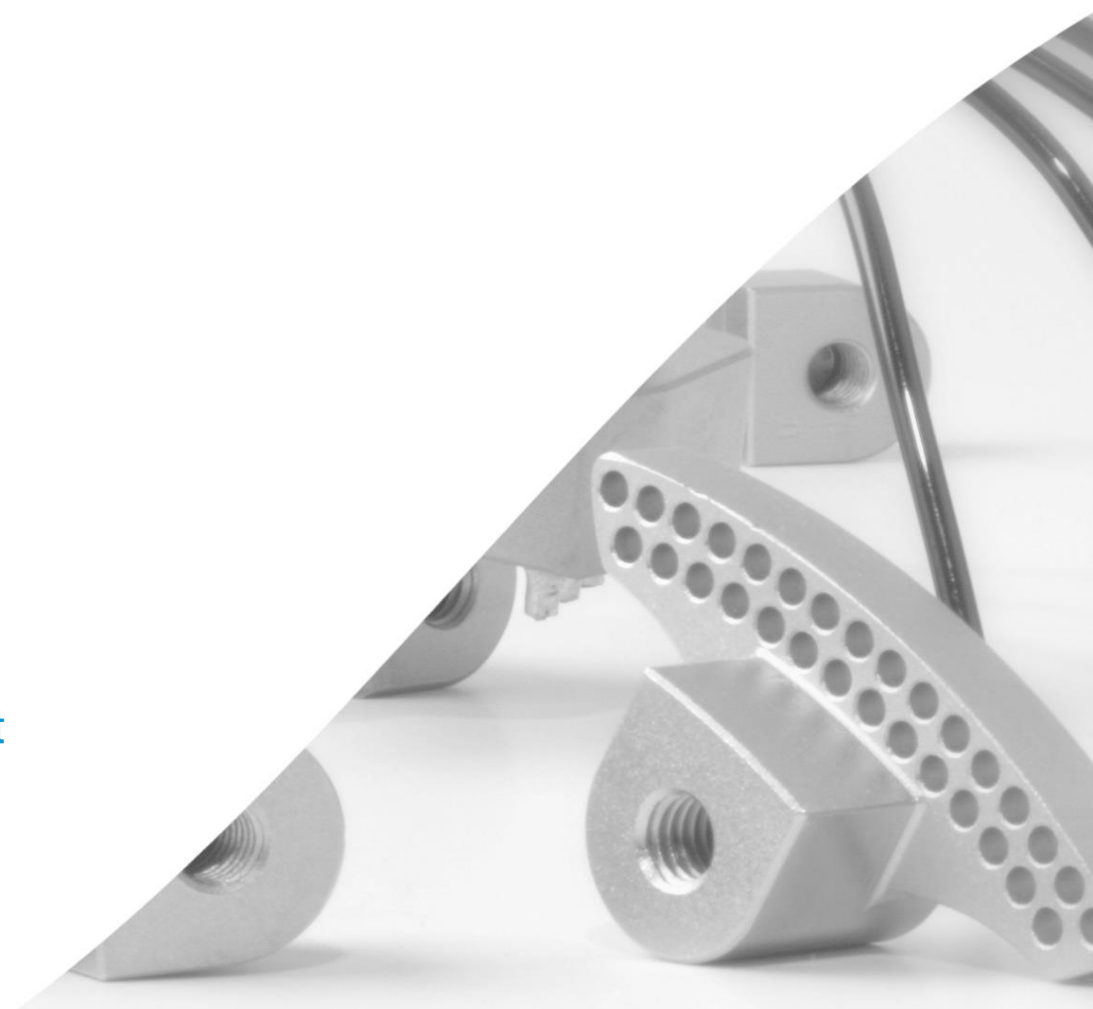


Winding with flat bar wire



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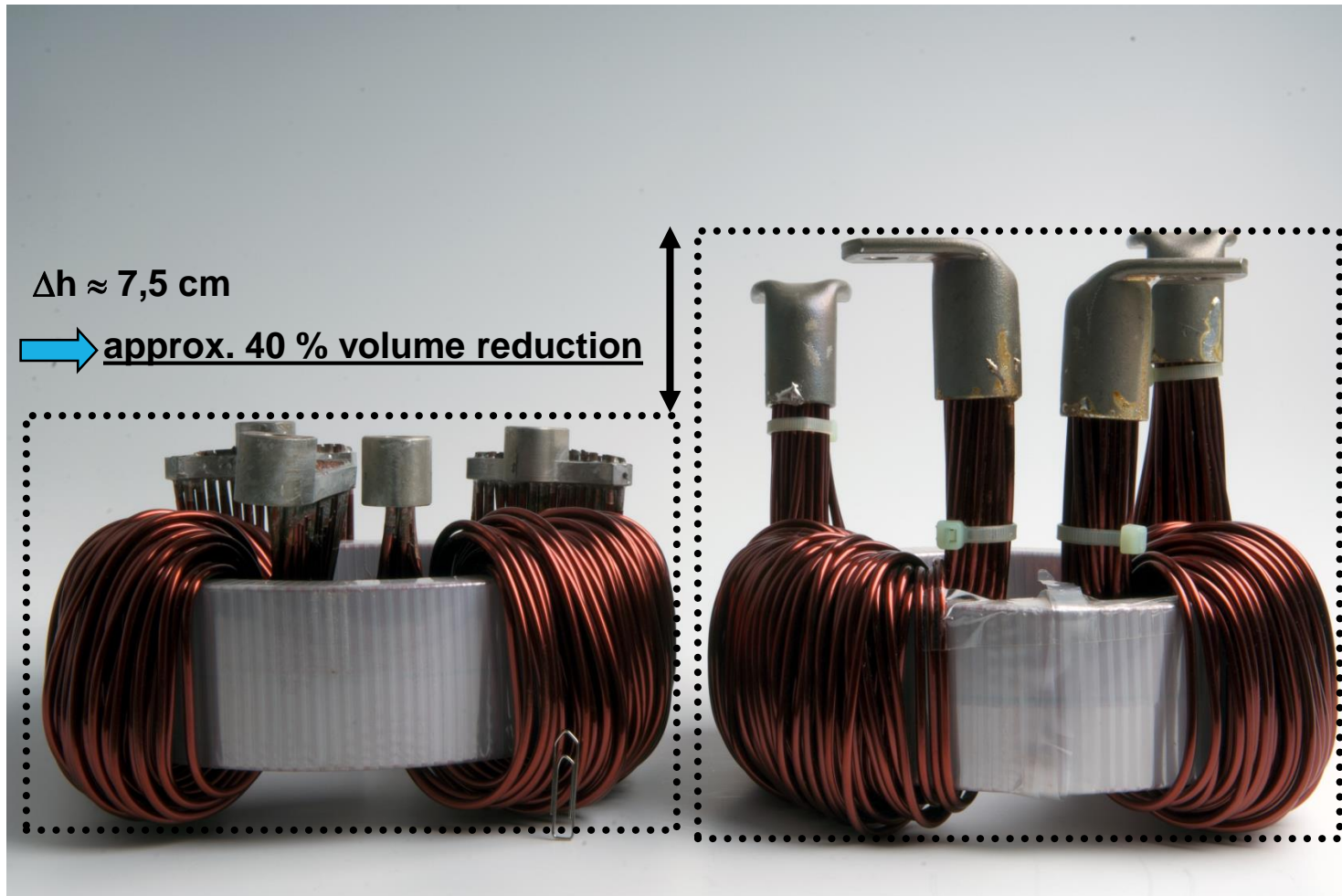
New contacting technique

$I_N=500\text{ A}$; $L= 2 \times 1000\ \mu\text{H}$

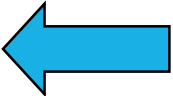


New contacting technique

$I_N=500\text{ A}$; $L= 2 \times 1000\ \mu\text{H}$



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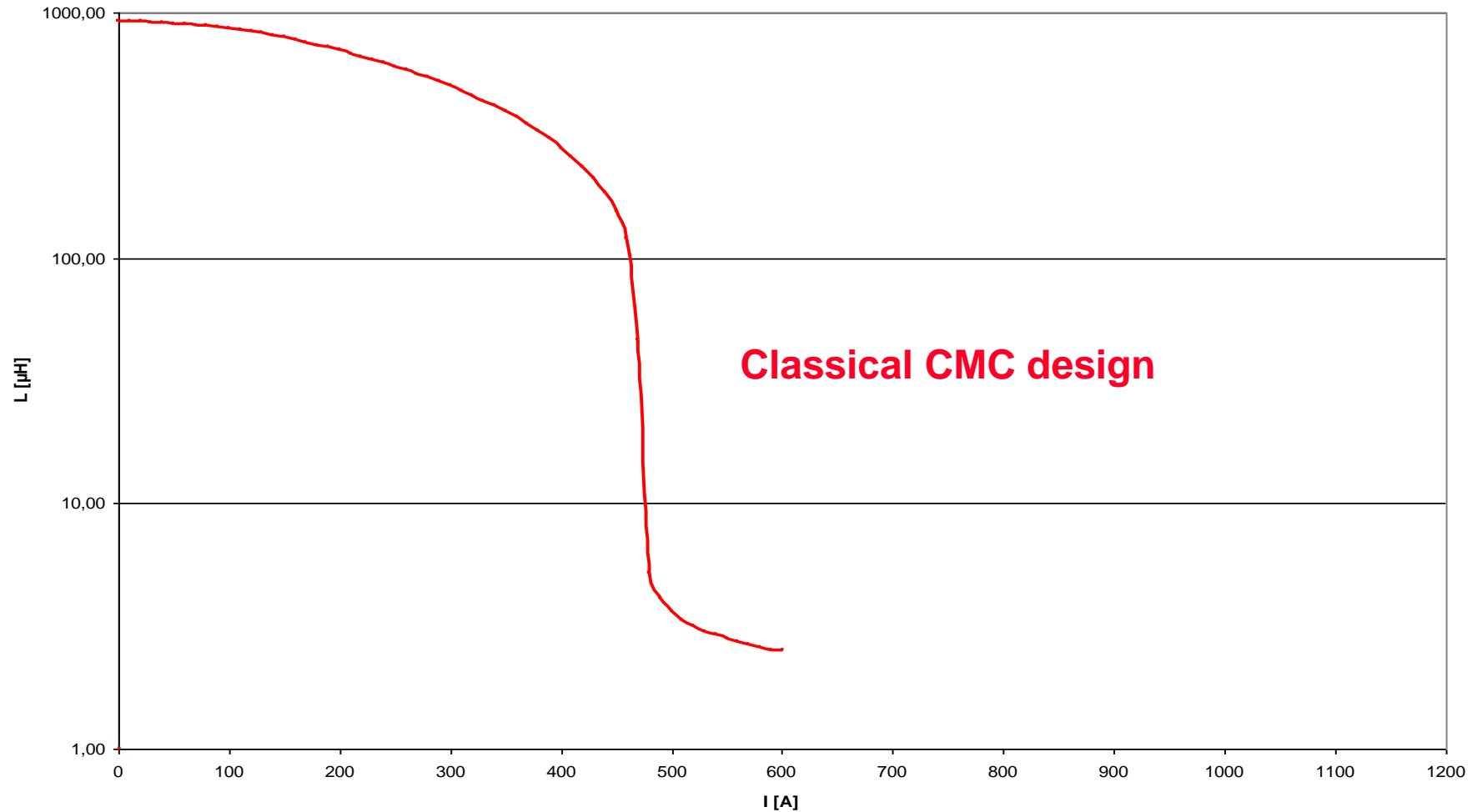


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Inductance vs. nominal current

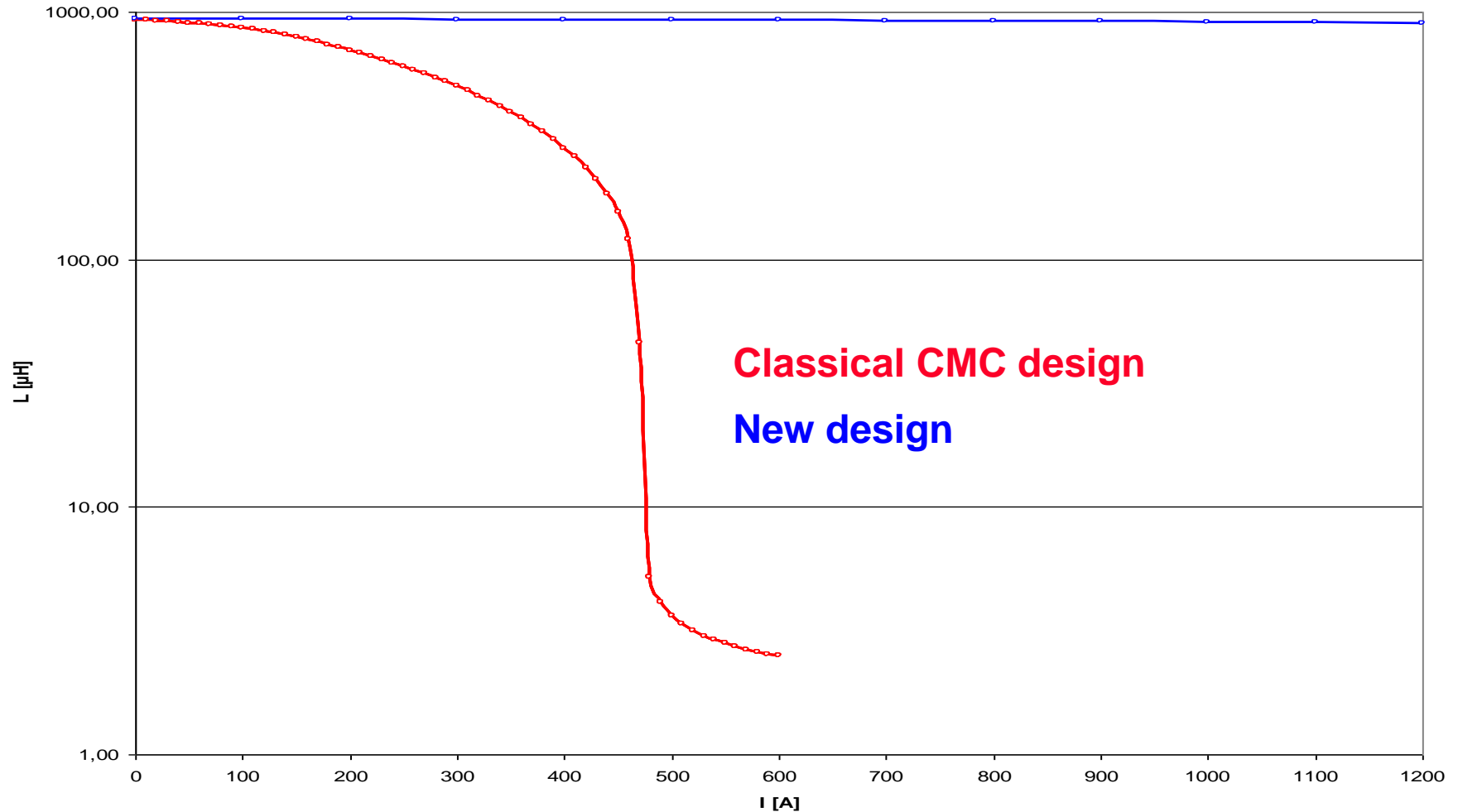
$$I_N = 300 \text{ A} / L = 2 \times 1000 \text{ } \mu\text{H}$$



Classical CMC design

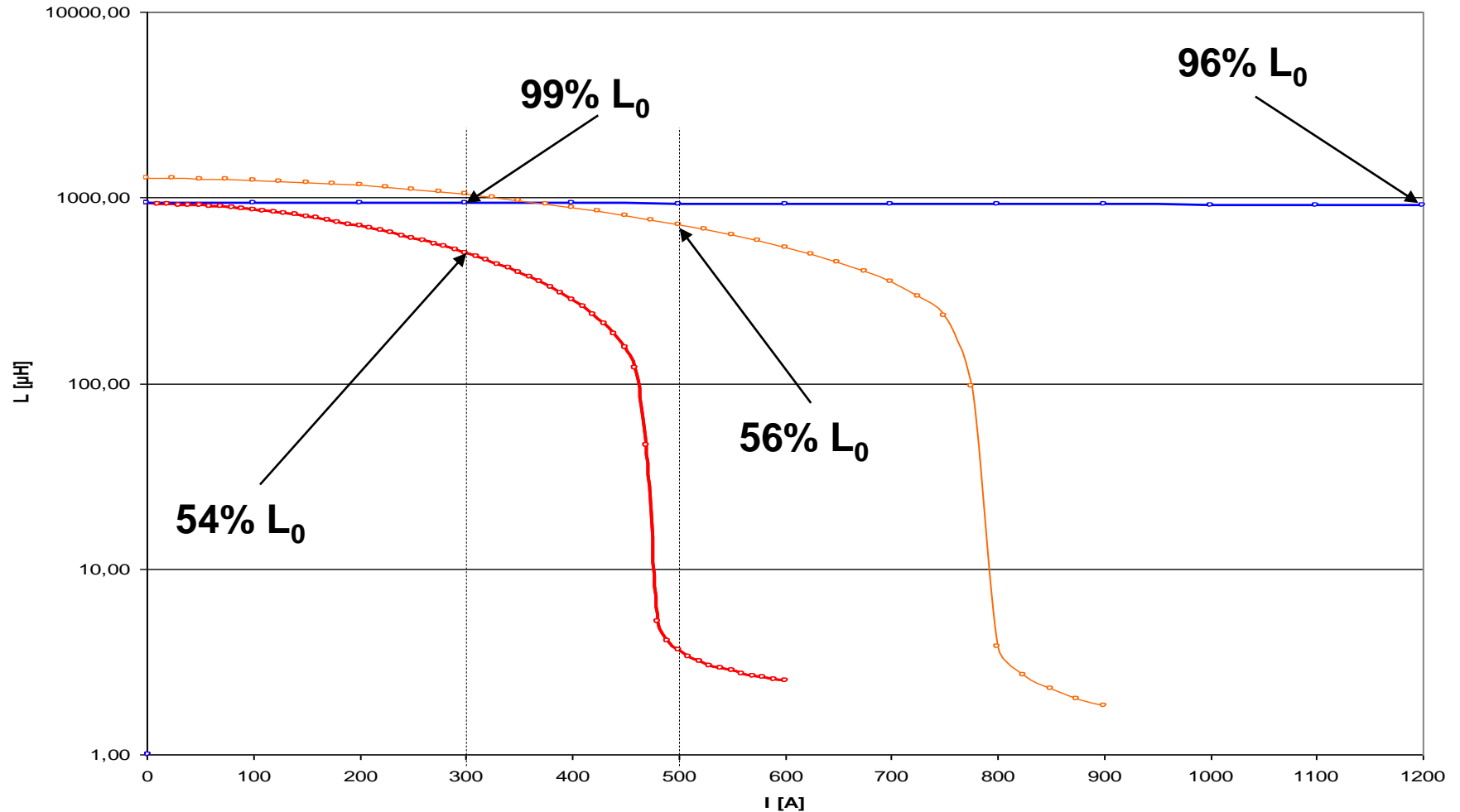
Inductance vs. nominal current

$$I_N = 300 \text{ A} / L = 2 \times 1000 \text{ } \mu\text{H}$$



Inductance vs. nominal current

$I_N = 300 \text{ A}$ und $500 \text{ A} / L = 2 \times 1000 \text{ } \mu\text{H}$



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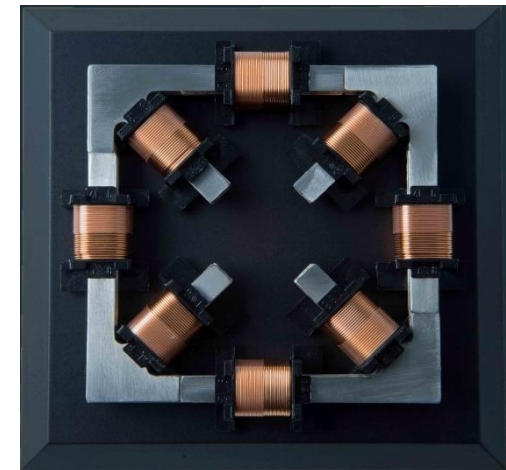


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Magnetic applications



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